ECE325 Advanced Photonics Light propagation in anisotropic crystals lesson 4

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Outline

1 Propagation of light in Uniaxial crystals

Applications to optical instruments

- Half-wave retarder plate
- Quarter-wave plate

3 Reference texts

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Exercise: consider a Uniaxial crystal with length L along z and optic axis in the plane (x, y). A plane wave with k parallel to \hat{z} impinges on the crystal. Calculate the emerging Electric field at the output of the crystal.



 \hat{n}_o and \hat{n}_e are unit vectors along the principal ordinary and extraordinary axes, respectively, while $\boldsymbol{E} = [E_x, E_y, 0]$ is electric input field.

For **k** parallel to *z*, the plane waves propagating in the uniaxial crystals have refractive index n_e and n_o , with polarization vectors parallel to \hat{n}_e and \hat{n}_o , respectively. To solve for the propagation of the electric field, we decompose the field along \hat{n}_e and \hat{n}_o :

$$\begin{bmatrix} E_x \\ E_y \end{bmatrix} = \begin{bmatrix} \cos\theta & -\sin\theta \\ \sin\theta & \cos\theta \end{bmatrix} \begin{bmatrix} E_o \\ E_e \end{bmatrix} \quad (1)$$

Each component E_e and E_o represents a plane wave solution inside the anisotropic crystal propagating with wavevector $\mathbf{k}_e = \frac{\omega}{c} n_e \hat{z}$ and $\mathbf{k}_o = \frac{\omega}{c} n_o \hat{z}$, respectively.



After a distance z = L in the uniaxial crystal, plane waves propagate as follows:

$$E_o(L) = E_o(0)e^{-ik_{oz}L} = E_o e^{-i\frac{\omega}{c}n_oL}$$
$$E_e(L) = E_e(0)e^{-ik_{ez}L} = E_e e^{-i\frac{\omega}{c}n_eL}$$
(2)

In matrix form, the last expression reads:

$$\begin{bmatrix} E_o(L) \\ E_e(L) \end{bmatrix} = e^{-i\frac{\omega}{c}L \cdot \underline{n}} \begin{bmatrix} E_o(0) \\ E_e(0) \end{bmatrix}, \qquad \underline{n} = \begin{bmatrix} n_o & 0 \\ 0 & n_e \end{bmatrix}$$
(3)

Due to birefringence, the two plane waves, originally having the same phase, acquire a phase delay $\Delta \phi = (n_o - n_e) \frac{\omega L}{c}$ at z = L.

It is convenient to write the propagation of the field as a function of the phase delay $\Delta\phi$:

$$\begin{bmatrix} E_o(L) \\ E_e(L) \end{bmatrix} = e^{-i\frac{1}{2}(n_e+n_o)\frac{\omega}{c}L} \begin{bmatrix} e^{-i\frac{\Delta\phi}{2}} & 0 \\ 0 & e^{i\frac{\Delta\phi}{2}} \end{bmatrix} \begin{bmatrix} E_o(0) \\ E_e(0) \end{bmatrix} = \underline{W} \cdot \begin{bmatrix} E_o(0) \\ E_e(0) \end{bmatrix}$$
(4)

At the output of the crystal, in order to get back to the original coordinates, we apply a rotation:

$$\begin{bmatrix} E_x(L) \\ E_y(L) \end{bmatrix} = \underline{\underline{R}} \cdot \underline{\underline{W}} \cdot \underline{\underline{R}}^{\dagger} \cdot \begin{bmatrix} E_x(0) \\ E_y(0) \end{bmatrix},$$
(5)

with:

$$\underline{\underline{R}} = \begin{bmatrix} \cos\theta & -\sin\theta\\ \sin\theta & \cos\theta \end{bmatrix}$$
(6)

defining a rotation matrix in the (x, y) plane.

The total input-output transfer matrix of the structure is then:

$$\underline{\underline{R}} \cdot \underline{\underline{W}} \cdot \underline{\underline{R}}^{\dagger} = \begin{bmatrix} e^{-i\frac{\Delta\phi}{2}}\cos\theta^2 + e^{i\frac{\Delta\phi}{2}}\sin\theta^2 & -i\sin\frac{\Delta\phi}{2}\sin2\theta \\ -i\sin\frac{\Delta\phi}{2}\sin2\theta & e^{-i\frac{\Delta\phi}{2}}\sin\theta^2 + e^{i\frac{\Delta\phi}{2}}\cos\theta^2 \end{bmatrix}$$
(7)

The approach used above to the model the propagation of electric field in anisotropic crystals is known as Jones Calculus, while the 2×2 transfer matrices that we used in the previous equations are known as Jones Matrices.

Exercise: verify that the transfer matrix is unitary, i.e., $\underline{T} \cdot \underline{T}^{\dagger} = \underline{1}$, with $\underline{1}$ being the identity matrix and $\underline{T} = \underline{R} \cdot \underline{W} \cdot \underline{R}^{\dagger}$. Advanced question: what is the physical interpretation of this result?

From a more general perspective, the approach we used to solve the propagation problem is based on eigenvalue decomposition:



and exploits the linearity of Maxwell equations. For nonlinear materials, this approach cannot be used and other strategies are employed based on more complex transforms.

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It is composed by a uniaxial crystal in the configuration studied in the previous exercise, with:

$$\Delta \phi = (n_e - n_o) \frac{\omega}{c} L = \pi, \quad (8)$$

The length of the crystal is then $L = \frac{\lambda}{2\Delta n}$, with $\Delta n = n_e - n_o$. In this system, when $\theta = \frac{\pi}{4}$, the transfer matrix \underline{T} reads:

$$\underline{\underline{T}} = -i \begin{bmatrix} 0 & 1 \\ 1 & 0 \end{bmatrix} = -i\sigma_1, \quad (9)$$

being σ_1 the Pauli matrix.



An x-polarized electric field at the beginning $\boldsymbol{E} = [1,0]$, transforms into:

$$\boldsymbol{E}(L) = -i\sigma_1 \boldsymbol{E} = -i \begin{bmatrix} 0\\1 \end{bmatrix}, \qquad (10)$$

which represents a y-polarized field at the output.



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July 3, 2021 11 / 17

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Exercise: calculate the evolution of a circular polarized electric field $\pmb{E}=\frac{1}{\sqrt{2}}[1,i]$

Advanced question: design a power controller by using an half-wave retarder.

Exercise: calculate the evolution of a circular polarized electric field $\boldsymbol{E} = \frac{1}{\sqrt{2}} [1, i]$

Advanced question: design a power controller by using an half-wave retarder. We can use a half-wave retarder plate followed by a polarizer. We can verify that the transfer matrix of a polarizer is:

$$\underline{\underline{P}}_{x} = \begin{bmatrix} 1 & 0\\ 0 & 0 \end{bmatrix}, \qquad \qquad \underline{\underline{P}}_{y} = \begin{bmatrix} 0 & 0\\ 0 & 1 \end{bmatrix}, \qquad (11)$$

for an x-polarizer and y- polarizer, respectively. If we orient the half-wave retarder plate at a generic θ , the transfer matrix becomes:

$$\underline{\underline{T}} = -i \begin{bmatrix} \cos 2\theta & \sin 2\theta \\ \sin 2\theta & -\cos 2\theta \end{bmatrix}$$
(12)

Consider a generic field at the input linearly polarized, in this example along x, $\boldsymbol{E} = [E_x, 0]$. At the output of the system crystal + polarizer, we have:

$$\begin{bmatrix} E_x(L) \\ E_y(L) \end{bmatrix} = \underline{\underline{P}}_x \cdot \underline{\underline{T}} \cdot \begin{bmatrix} E_x \\ 0 \end{bmatrix} = \begin{bmatrix} E_x \cos 2\theta \\ 0 \end{bmatrix}, \quad (13)$$

as a result, the output intensity $I = |\mathbf{E}|^2 = |E_x|^2 \cos 2\theta^2$ cab be modulated between 0 and $|E_x|^2$ by simply acting on the rotation angle of the crystal. When $\theta = \frac{\pi}{4}$, the output intensity is 0, as expected. In this condition, in fact, the half-wave retarder rotates the input polarization and the polarizer prevents the beam to pass through the system.

Quarter-wave retarder plate

It is composed by a uniaxial crystal with:

$$\Delta\phi = (n_e - n_o)\frac{\omega}{c}L = \frac{\pi}{2}, \quad (14)$$

The length of the crystal is then $L = \frac{\lambda}{4\Delta n}$, with $\Delta n = n_e - n_o$. In this system, when $\theta = \frac{\pi}{4}$, the transfer matrix \underline{T} reads:

$$\underline{\underline{T}} = \frac{1}{\sqrt{2}} \begin{bmatrix} 1 & -i \\ -i & 1 \end{bmatrix}$$
(15)

This transforms linearly polarized beams into circularly polarized light and vice-versa.



Retarder plates

Advanced question: A student is investigating the propagation of light in a system composed by two polarizers in cross configuration. Due to this configuration, no light is expected to emerge from the system. However, the student observes that if he puts a half-retarder plate in between the two polarizers, some light emerges from the system. Explain the phenomenon.

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